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COMPARE DOCUMENT

## DISPLACEMENT DEVICE

### 5 CROSS-REFERENCE

This application claims priority of German Application No. 199 26 994.7 filed ~~8 June 1999~~, ~~a copy of which is Attachment A hereto, the disclosure of which is incorporated fully herein by reference.~~ June 8, 1999. This application is also a continuation of patent Application No. 09/592,485, filed June 8, 2000, the disclosure of which is incorporated fully herein by reference.

### 15 DESCRIPTION

#### BACKGROUND OF THE INVENTION

The invention relates to a displacement device ~~according to the preamble of claim 1.~~

From DE 41 20 617 C2 a displacement device is known which has a load torque lock with which torque on the drive side is transferred in both directions to an output element ~~while~~ while torque on the output side is blocked in both directions by the load torque lock and the force is introduced into a displacement housing and is consequently not transferred to the drive element.

Between the drive element and the load torque lock the torque on the drive side is transferred by means of elements which engage in each other with keyed engagement. Since the position of the locking elements of the load torque lock changes through tolerances and wear as a result of high flat surface pressures, in order to reach the required functional reliability of the known displacement device it is necessary to incorporate a large play so that during functioning a torsion angle play is present between the interengaging

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elements without which a stepped transfer or change of direction of the torques on the drive side is not possible. A minimum torsion angle play must also therefore be present between the interengaging elements of the drive element and the load torque lock in order to guard against wear and enable a certain elastic deformation.

Opposite this however too much torsion angle play, particularly in the case of a stepped transfer of the torque on the drive side, has a noticeable detrimental effect since the torsion angle play causes a correspondingly large idling path or idling stroke of the drive element. Furthermore too much torsion angle play can lead, when reversing the movement, to a detrimental reversal play and to inaccurate handling.

The known displacement device has a relatively large reversal play in the brake unit conditioned by the tolerances of the structural parts. In order to restrict this, manufacture must be carried out precisely within a narrow tolerance band. The assembly of the individual component parts which are provided with small tolerances is therefore expensive since the component parts which are to be connected together have to be positioned very precisely relative to each other.

#### SUMMARY OF THE INVENTION

The object of the present invention is therefore to provide a displacement device with optimum torsion angle play between a drive element, an output element and a load torque block which on the one hand is restricted to a minimum and on the other ensures a reliable force and torque transfer and which during assembly requires no adjustment and even after long term use requires no adjustment of the torsion angle play.

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5       ~~This is achieved according to the invention through a displacement device having the features of patent claim 1.~~

10       According to the invention a play compensating device which balances the torsion angle play between the drive element, output element and the load torque block, is mounted between the drive element and the load torque block or between the output element and the load torque block so that the functionally-conditioned torsion angle play between the drive element and the load torque lock or between the load torque lock and the output element is set and adjusted automatically. An automatic setting of the optimum torsion angle play thereby takes place taking into account the tolerances of the component parts and the adjustment is carried out taking into account the wear on the component parts so that a minimum idling stroke is ensured during operation and a high functional reliability of the displacement device is ensured taking into account the unavoidable wear. The manufacture of the individual component parts is thus considerably more economical, assembly of the displacement device is simplified and rejects are restricted to a minimum.

20       The load torque lock preferably has at least two locking elements mounted in a cylindrical displacement housing, with the clamping faces of the locking elements acting with predetermined pretension on the displacement housing under the action of the play compensating device which is mounted at least in part between opposing expanding faces of the locking elements and presses these locking elements apart from each other. Torque introduced on the output side thereby increases the bearing force of the clamping faces and thus of the locking elements against the displacement housing.

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      The play compensating device can be guided in the drive  
element and can be connected to a spring which pretensions the  
5       play compensating device in the play compensating direction  
~~whilst~~while the locking elements are loaded with pretensioning  
force against the play compensating direction.

      The play compensating device can be formed in different  
ways in order to ensure the locking elements bear on the  
10       displacement housing with the predetermined pretensioning  
force and in order to guarantee an automatic adjustment which  
becomes necessary as the component parts wear down. In a  
first embodiment the play compensating device consists of at  
least one wedge mounted between the expanding faces of the  
15       locking elements, where the wedge faces oppose the expanding  
faces of the locking elements and where the wedge is guided  
displaceable with a wedge guide in keyed connection in a slide  
guide of the drive element and is pretensioned radially by  
means of a spring so that the wedge faces adjoin the expanding  
20       faces free of play.

      In order to ensure that the wedge on the one hand in the  
absence of any drive torque engenders the optimum setting and  
adjustment and does not hinder the movement of the locking  
elements, but on the other hand in the event of torque on the  
25       drive side is not radially displaced by the locking elements,  
and in order to keep the system able to function in the widest  
possible range, the material matching of the expanding faces  
and of the wedge faces on the one hand and of the active faces  
of the wedge guide and the slide guide of the drive element on  
30       the other hand is predetermined so that with the absence of  
drive torque the expanding faces can move the wedge against  
the action of the spring, but in the event of load on the  
drive side the wedge is held in its position. This is caused  
for example by a small friction value between the wedge faces

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and the expanding faces as well as by a high friction value between the guide face of the wedge and the slide guide of the drive element.

As an alternative or in addition the displacement device or the play compensating device can be geometrically designed so that the wedge angle  $\alpha$  which the wedge faces include between themselves, the minimum friction angle  $\sigma_{sperr,min}$  in the event of load on the drive side and the maximum friction angle  $\sigma_{sperr,max}$  in the event of load on the output side between the wedge faces and the expanding faces as well as the minimum friction angle  $\sigma_{antr,min}$  between the wedge guide and the slide guide meets the conditions

$$2 * \sigma_{sperr, max} < \alpha$$

$$\sigma_{antr, min} + \sigma_{sperr,min} > \alpha/2$$

in which  $\sigma = \arctan \mu$  and  $\mu$  is the friction value between the friction faces formed from the surface pairings wedge surface/expanding surface and wedge guide/ slide guide.

In order to intensify the clamping action of the wedge the wedge guide can be arranged radially off-set from the expanding faces of the locking elements. A reduction of the (radial) height of the wedge also leads to an intensification of the clamping action so that when necessary the wedge angle can also be selected as obtuse.

In order to produce a defined spot or linear contact between the wedge and the expanding faces of the locking elements, the expanding faces of the locking elements or the wedge faces are formed ball-shaped so that the slide action is minimal as a result of the slight friction of the surfaces which slide on each other and thus easy adjustment is guaranteed.

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          In a second embodiment the play compensating device consists of at least one cylindrical roller or ball mounted  
5       between the expanding faces of the locking elements, wherein the roller or ball guide is mounted in a slide guide of the drive element and its outer face adjoins with linear or spot contact against the flat or ball-shaped expanding faces of the locking elements free of play.

10       In a third embodiment the play compensating device consists of at least one eccentric mounted rotatable between the expanding faces of the locking elements and preferably formed as a stepped bolt, with an eccentric stud mounted in a bore of the drive element and is radially pretensioned by a  
15       torsion spring so that the eccentric faces adjoin the expanding faces of the locking elements free of play.

          Through the shaping and/or surface conditions the eccentric faces adjoin the expanding faces of the locking elements and the eccentric stud is connected to the drive  
20       element so that when the drive element is actuated the eccentric is blocked and does not obstruct the movement of the locking elements.

          An automatic compensation of the optimum torsion angle play can be provided with different structural forms of the displacement device or drive element, output element and the  
25       load torque lock ~~according to the features of sub claims 14 to 29.~~ These embodiments comprise inter alia the arrangement of pairs of locking elements in two superposed planes, applying a pretensioning force to the play compensating device by means  
30       of compression, yoke or formed springs, with or without additional force transfer elements, such as shears and the like and the positive-locking torque transfer from the drive element to the output element when the locking action is lifted through the load torque lock.

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BRIEF DESCRIPTION OF THE DRAWINGS

Further advantages are produced from the following described embodiments in which:

Figures 1 to 7 which consists of Figs. 2a-2c, Figs. 3a-3b, and Figs. 7a-7b show diagrammatic illustrations for explaining the functioning principle of different play compensating devices for displacement devices with a load torque lock;

Figure 8 shows a cross-sectional view through a load torque lock with wedges guided in the drive element for adjusting brake elements;

Figure 9 shows a cross-sectional view through a load torque lock with wedges guided in the drive element and with scissor arms for adjusting locking elements;

Figure 10 shows a plan view and

Figure 11 shows a longitudinal sectional view through a load torque lock with wedges guided in the drive element and wire springs connecting these together as pretensioning elements;

Figure 12 shows a load torque lock according to Figures 10 and 11 with a yoke or formed spring between the wedges adjusting the locking elements;

Figures 13 and 14 show a load torque lock with wedges connected by springs and adjoining the end faces of the locking elements in the case of different play;

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Figures 15 and 16 show a load torque lock with wedges connected by springs and enclosed by the locking elements with different play; Figure 17 shows a load torque lock with rod-like drive element guided through the output element and the wedge of a play compensating device, and Figure 18 shows a load torque lock as in Figure 17 with a rod-like drive element which is pushed through a bore of the output element and onto the end of which is pushed a wedge of a play compensating device.

The diagrammatic illustrations of the load torque locks in Figures 1 to 7 serve only to explain the functioning principle of play compensation for displacement devices. Figures 8 to 18 show various different embodiments for concrete designs of displacement devices and play compensating devices used therein. The reference numerals used in the function illustrations of Figures 1 to 7 as well as the reference numerals used to designate the individual parts of the displacement devices in the concrete embodiments of Figures 8 to 18 coincide where they relate to the same or similar functioning component parts. The alphabetical additions to the reference numerals similarly designate the same or similar type of functioning elements of the various embodiments.

#### DETAILED DESCRIPTION OF THE INVENTION

Figure 1 shows a front sectional view through a double-sided acting displacement device 1a with a displacement housing 10 in which the functional parts of a load torque lock



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are mounted with automatic play compensation. FIG. 1a shows  
a side sectional view. A drive element formed as a drive  
5 lever 2a is mounted rotatable about an output axle ~~30 which~~30.  
The output axle 30 includes an axis E about which the drive  
lever rotates in direction D. The output axle 30 is connected  
to an output element 3a. Between the drive element 2a and the  
10 output element 3a there are locking elements 4a and 4a' formed  
as segments and adjoining the cylindrical inner face of the  
displacement housing 10 with a part of their peripheral faces  
42a, 42a' which are formed as locking faces 43a and 43a'.

The opposing expanding faces 41a, 41a' of the locking  
elements 4a and 4a' are adjoined by wedge faces 51a and 51a'  
15 of a wedge 5a which causes an automatic play compensation.  
The wedge 5a is mounted with a wedge guide 52a in a recess 20a  
of the drive lever 2a formed as a wedge slide guide and is  
pretensioned by means of a spring 7a so that the wedge faces  
51a, 51a' press in ~~the~~a play compensating direction c, c'  
20 circular against the expanding faces 41a, 41a' of the locking  
elements 4a, 4a' and thus bring the locking faces 43a, 43a' of  
the locking elements 4a, 4a' to bear against the cylindrical  
inner face of the displacement housing 10.

The locking elements 4a, 4a' are pretensioned by a  
25 locking element spring 6a, circular against the play  
compensating direction c, c' so that the expanding faces 41a,  
41a' endeavour to press the wedge 5a out from the interspace  
between the expanding faces 41a and 41a'. As explained in  
further detail below from the enlarged detailed illustration  
30 of the play compensating device according to Figures 2a to 2c  
the friction conditions between the expanding faces 41a, 41a'  
and the wedge faces 51a, 51a' on the one hand and the wedge  
guide 52a and the wedge slide guide 20a on the other hand are  
produced so that when torque is applied on the drive side the

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locking elements 4a, 4a' are entrained free of play by the wedge 5a, but on the other side the locking elements 4a and 4a' are dragged without hindrance by the wedge 5a for play compensation, i.e. in the rest state are pressed through the wedge 5a under the action of the spring 7a with their locking faces 2343a, 2343a' against the displacement housing 10.

This function conditions a small friction value at the friction face formed between the wedge faces 51a, 51a' and the expanding faces 41a, 41a' and a large friction value at the friction face formed between the wedge guide 52a and the wedge slide guide 20a so that under certain geometric conditions the wedge 5a is prevented from being pressed out from the interspace between the expanding faces 41a, 41a'.

When torque is introduced on the drive-side through the drive lever 2a the torque is transferred through the wedge 5a to the expanding faces 41a or 41a' of the locking elements 4a or 4a' depending on the direction of rotation and the locking elements 4a or 4a' are entrained in the circumferential direction since the bearing contact of the locking faces 43a, 43a' of the locking elements 4a, 4a' against the cylindrical inner face of the displacement housing 10 is not sufficient to block the torque which is introduced. Gaps F, F' are provided between lower portions of the locking elements 4a, 4a' and the output element 3a. After the locking element 4a, 4a' has been moved slightly in the circumferential direction through the torque introduced on the drive side, ~~the~~claw slide guides 21a and 21a' of the drive lever 2a come into positive-locking engagement with claws 31, 32 on the output side and entrain the output element 3a in keyed engagement into the relevant rotary direction of the drive lever 2a. ~~An additional~~A keyed connection between the drive element 2a and output element 3a of this kind which is activated after a slight rotation has

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been introduced and transfers the further transfer of the torque exerted by the drive element 2a to the output element 3a, is however not absolutely necessary since the transfer of the torque from the drive element 2a to the output element 3a can also take place through the wedge 5a of the play compensating device and through the locking elements 4a, 4a' to the output element 3a. The half of the inner face 44a, 44a' of the locking element that extends in the direction of the spring 6a closes the gap F, F' and abuts against the output element 3a to transmit the drive torque.

With the introduction of torque on the output side depending on the direction of rotation the outer face of the output element 3a is loaded more heavily at points A or A' and presses the inner locking element faces 44a, 44a' radially apart so that the locking faces 43a or 43a' intensify their bearing contact against the cylindrical inner face of the displacement housing 10 and thus block the torque introduced on the output side.

Figure 2a shows in an enlarged detailed illustration of Figure 1 a play compensating device with a wedge 5a as the play compensating element and a section of the drive lever 2a with wedge slide guide 20a provided therein as a recess in which the wedge guide 52a of the wedge 5a is mounted and adjoins with keyed engagement against the side walls of the wedge slide guide 20a of the drive lever 2a running perpendicular to the drive direction, but is displaceable perpendicular to the drive direction inside the wedge slide guide 20a.

The wedge faces 51a and 51a' of the wedge 5a are adjoined by the expanding faces 41a and 41a' of the locking elements 4a, 4a'. In order to actuate the locking elements 4a, 4a' connected in force-locking engagement with the output element

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3a the wedge 5a is guided in the drive element 2a with the  
wedge guide 52a and biased with a compression spring 7a so  
5      that the wedge faces 51a and 51a' adjoin free of play the  
expanding faces 41a, 41a' of the locking elements 4a, 4a'  
without being pressed apart against a spring which may be  
present (for example the locking element spring 6a according  
to Figure 1) or the locking elements 4a, 4a' lifting off from  
10      the cylindrical inner wall of the displacement housing 10.

Figure 2b shows the force and friction conditions in the  
event of load on the drive side, i.e. with the action of the  
drive element 2a on the wedge 5a. In the event of entrainment  
of the wedge 5a through the drive element 2a against a side of  
15      the locking element 4a or 4a',  $\alpha/2$  acts as the wedge angle.  
In the event of a force equilibrium, i.e. in the blocking  
state

$$(1) \sigma_{antr} + \sigma_{sperr} = \alpha/2.$$

20      In order to ensure a secure hold, the sum of the friction  
values when the wedge 5a slips through must however be larger  
than the wedge angle  $\alpha/2$  so that in the event of load on the  
drive side the following applies

$$(2) \sigma_{antr, \min} + \sigma_{sperr, \min} > \alpha/2$$

25      in which

$\sigma_{sperr, \min}$  is the minimum friction angle and  $\sigma_{sperr, \max}$  is the  
maximum friction angle between the wedge faces 51a and the  
expanding faces 41a,  $\sigma_{antr, \min}$  the minimum friction angle between  
30      the wedge guide 52a and the wedge slide guide 20a,  $\sigma = \arctan \mu$   
and  $\mu$  is the friction value between the friction faces  
formed from the surface pairings wedge face/expanding face and  
the wedge guide/slide guide.

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Figure 2c shows the forces and friction angle in the event of load on the output side, i.e. in the event of load on the side of the locking elements 4a or 4a'. In this case of load on the wedge 5a free of drive torque from the sides of the locking element 4a or 4a', the sum of the limit friction values must be

$$(3) \quad 2 * \sigma_{\text{sperr, max}} < \alpha$$

so that the wedge 5a does not impede the movement of the locking elements 4a, 4a'. If this condition is fulfilled the wedge 5a slips through without any drive torque as a result of force exerted by the locking elements 4a, 4a', ~~whilst~~while it is blocked in the event of force exerted by the drive element 2a on the locking elements 4a, 4a'.

So that the system functions in the largest possible range of  $\sigma_{\text{sperr}}$  it is advantageous to make  $\sigma_{\text{antr, min}}$  as large as possible, e.g. by providing corresponding roughness or mini-serrations.

~~Figure 3 shows~~ Figures 3a and 3b show a possibility of intensifying the self-locking effect of a wedge 5b to guard against the wedge 5b being pressed out through the action of the expanding faces 41b, 41b' of the locking elements 4b, 4b' on the wedge 5b by providing a contact bearing for the wedge 5b at two points through canting. This is achieved through an eccentric arrangement of the wedge guide 52b in relation to the expanding faces 41b, 41b' of the locking elements 4b, 4b' wherein the height H of the wedge guide 52b and the distance s of the upper edge of the wedge guide 52b from the contact point of the expanding faces 41b, 41b' is variable.

With a decrease in the height H or through an increase in the distance s the canting effect is intensified so that the wedge angle  $\alpha$  of the wedge 5a can become more obtuse. In the

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event that the distance  $s$  is equal to zero then the arrangement exists according to the method of operation of Figure 2. With an increasing distance  $s$  through the off-set wedge guide an intensifying canting effect is produced which increases the contact bearing force and hinders the system from slipping through in the event of drive load with significantly smaller friction angles. With a predetermined wedge angle  $\alpha$  the minimum height  $H$  of the wedge guide 52b and thus a minimum distance  $s$  of the centre of the wedge guide 52b from the centre of the expanding faces 41b, 41b' of the locking elements 4b, 4b' must be provided in order to guarantee the functioning of the play compensating device.

Figure 34 shows a ball-shaped design of the expanding faces 41c, 41c' of the locking elements 4c, 4c' wherein the wedge faces 51c, 51c' fix the angle for the geometric conditions described above. As an alternative the wedge faces 51c and 51c' can be made ball-shaped and the expanding faces 41c, 41c' of the locking elements 4c, 4c' can be flat.

Figure 5 shows a function diagram in which instead of a wedge as with the displacement device described above, a cylinder or a ball is provided as the play compensating element 5d and is guided analogous with the embodiments described above with a guide 5352d in a slide guide 20d of the drive element 2d. The play compensating element 5d lies with its cylinder or ball surface 51d against the expanding faces 41d, 41d' of the locking elements 4d, 4d'.

Figure 6 shows a displacement device 1e which corresponds to the displacement device 1a according to Figure 1. As opposed to the displacement device 1a according to Figure 1 here however a play compensating device is provided in the form of an eccentric 5e which is designed as a stepped bolt pretensioned with a torsion spring and mounted with a guide

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pin 52e in a bore 20e of the drive element formed as a drive lever 2e, the eccentric adjoining by its eccentric faces 51e the expanding faces 41e and 41e' of the locking elements 4e, 4e'.

Figures 7a and 7b show on an enlarged scale details of the play compensating device according to Figure 6 and the geometric conditions which are essential for the functioning of the play compensating device in the event of load on the output side (Figure 7a) on the part of the locking elements and in the event of load on the drive side (Figure 7b) on the part of the drive element 2e. The spring tensioning of the eccentric 5e is entered in the direction of the arrow  $F_{EF}$ .

The contact and friction conditions of the play compensating device shown in Figures 6, 7a and 7b are designed so that the eccentric 5e is blocked when the drive element 2e is actuated but does not obstruct the movement of the locking elements 4e and 4e' which is necessary for a satisfactory locking of torque introduced on the output side, even when taking into account wear on the component parts.

According to Figure 7a the contact bearing points between the eccentric 5e and the locking elements 4e, 4e' are designed so that in the event of load through the locking elements 4e and 4e' a relatively large angle  $\alpha_{sp \max}$  is produced between the force direction of the contact points and the horizontal which is greater than the maximum friction angle so that in the event of load on the output side the eccentric 5e can be turned back by the locking elements 4e, 4e' against the pretensioning force  $F_{EF}$  of the eccentric 5e.

With the conditions illustrated in Figure 7b, on the other hand, in the event of load on the drive side a minimum friction angle  $\alpha_{sp \min}$  is produced ~~on the other hand~~ between the expanding faces 41e and 41e' of the locking element 4e, 4e'

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and the eccentric 5e which prevents the eccentric 5e from turning back and thus ensures a direct and play-free force transfer. The friction area between  $\alpha_{sp} \alpha_{sp \min}$  and  $\alpha_{sp \max}$  is the friction area in which the friction values of the surface bearing between the eccentric and the locking elements have to lie for a functioning of the system. The force engagement point between the drive element and the bearing of the eccentric is produced from the force direction of  $\alpha_{sp \min}$ . The friction value between these faces must thereby be such that the slip through friction angle  $\sigma = \arctan \mu$  is greater than the angle  $\alpha_{antr \min}$  between this force direction and the normal to the circle, i.e. the bearing of the eccentric in the drive must be made consciously rough.

In other words: If the locking elements 4e, 4e' are compressed together then the eccentric 5e has to turn away, from which a maximum angle  $\alpha_{sp \max}$  results. All the friction angles must therefore be smaller than  $\alpha_{sp \max}$  so that the eccentric 5e can slip away.

Figures 8 to 19 illustrate various different variations of the load torque locks for displacement devices in which the functionally conditioned torsion angle play between the drive element and load torque lock is automatically set and adjusted.

For this purpose Figures 8 to 16 show embodiments for load torque locks with locking elements mounted in two planes for each of the two torsion directions of the displacement device, ~~whilst in~~ while Figures 17 ~~to 24~~ and 18 show embodiments ~~are shown~~ for load torque locks with locking elements mounted in one plane for each of the two turning directions of the displacement device.

The part of a displacement device shown in Figure 8 having automatic compensation of the functionally conditioned



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torsion angle play has on the drive side a follower disc 2f which is mounted rotatable inside a displacement housing 10 and is connected to a drive lever (not shown) which can swivel in one or other rotary direction and engenders a corresponding rotary movement of the follower disc 2f in one or other rotary direction. The follower disc 2f has diametrically opposite window-shaped openings 21f, 21f' in which claws 31f, 32f project ~~from~~ an output element 3f which is rotatable about a rotary axis of the output axle 30 and to which torque is transferred which is exerted on the follower disc 2f.

The load torque lock 1f contains in two superposed planes two pairs of segment type locking elements 4f, 4f' and 4f'', 4f''', between whose opposing chord faces 45f, 45f' and 45'', 45''' is mounted the output element 3f. The output element 3f and the locking elements 4f, 4f' and 4f'', 4f''' thereby contact one another when torque is introduced on the output side at points A, B' and B, A' dependent on the rotary direction of the output element 3f.

The claws 31f, 32f on one side and the expanding faces 41f, 41f' and 41f'', 41f''' of the locking elements 4f, 4f' and 4f'', 4f''' are adjoined in each plane of the locking elements 4f, 4f' and 4f'', 4f''' by locking element springs 6f, 6f' which consist of a W-spring and a compression spring mounted to reinforce the W-spring at the ends adjoining the expanding faces 41f, 41f' and 41f'', 41f''' of the locking elements 4f, 4f' and 4f'', 4f'''. The springs 6f, 6f' cause the locking elements 4f, 4f' and 4f'', 4f''' to adjoin both the output element 3f and also with their clamping faces 43f, 43f' and 43f'', 43f''' which are part of the peripheral faces 42f, 42f' and 42f'', 42f''' of the locking elements 4f, 4f' and 4f'', 4f''' with larger diameter, the displacement housing 10.

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      The angled ends of two scissor arms 81f, 82f are mounted  
in peripheral recesses of the locking elements 4f, 4f' and  
5       4f'', 4f''' and each radially adjoin radial stops 46f (of  
which only the radial stop of the one locking element 4f was  
marked) of the locking elements 4f, 4f' and 4f'', 4f''' in the  
two planes. This contact bearing is caused by wedges 5f, 5f'  
10       which are guided in diametrically arranged slit-like slide  
guides 20f, 20f' of the follow disc 2f by means of wedge  
guides 52f, 52f' and adjoin with their wedge faces 51f, 51f'  
on both sides the side contact bearing faces of the scissor  
arms 81f, 82f.

      Springs 7f, 7f' between the displacement housing 10 and  
15       the end faces of the wedges 5f, 5f' facing the displacement  
housing 10 press the wedges 5f, 5f' in the direction of the  
output axis 30 and thus cause the scissor arms 81f, 82f to  
spread apart so that these adjoin with their angled ends  
against the radial stops 46f of the locking elements 4f, 4f'  
20       and 4f'', 4f'''. For this purpose the springs 7f, 7f' are  
formed only strong enough so that they spread the scissor arms  
81f, 82f apart so that their angled ends bear against the  
radial stops 46f of the locking elements 4f, 4f' and 4f'',  
4f''' but not so the locking elements 4f, 4f' and 4f'', 4f'''  
25       can turn against the action of the locking element springs 6f,  
6f'.

      The slide guides 20f, 20f' of the follower disc 2f for  
housing the wedge guides 52f, 52f' have a rough or ribbed  
surface so that a self-locking bearing of the wedges 5f, 5f'  
30       in the slide guides 20f, 20f' of the follow disc 2f is  
ensured. On the other hand the contact bearing of the wedges  
5f, 5f' on the side contact bearing faces of the scissor arms  
81f, 82f has no self-locking action, i.e. when the scissor  
arms 81f, 82f are compressed in the direction of the wedges

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5f, 5f' the wedges 5f, 5f' would be pressed outwards, i.e. in the direction of the displacement housing 10. The wedge faces 51f, 51f' or the side contact bearing faces of the scissor arms 81f, 82f are preferably provided with a ball-shaped surface in order to produce a linear contact between the contact bearing faces of the scissor arms 81f, 82f and the wedge faces 51f, 51f' of the wedges 5f, 5f'.

10       The wedge angle  $\alpha$  - as already explained in connection with Figures 1 to 4 - is measured so that the wedges 5f, 5f' are not moved outwards when loaded, i.e. towards the displacement housing 10.

15       In the rest state the locking elements 4f, 4f' and 4f'', 4f''' are pressed apart under the action of the locking element springs 6f, 6f' in each plane of the locking elements 4f, 4f' and 4f'', 4f''' and turned in the displacement housing 10 so far in the circumferential direction or circular until they adjoin both with their clamping faces 43f, 43f' and 43f'', 43f''' against the displacement housing 10 and against the points A and B or A' and B' respectively on the output element 3f. If torque is exerted on the follower disc 2f against the output torque M recorded by the curved arrow, then the follower disc 2f presses through the slide guides 20f, 20f' the wedge guides 52f, 52f' and the wedge faces 51f' against the scissor arm 81f which turns the locking elements 4f and 4f''' unloaded on the output side in the drive direction before the drive torque acts through the window-shaped recesses 21f, 21f' in the follower disc 2f on the claws 31f, 31f' of the output element 3f and causes a corresponding rotary movement of the output element 3f.

30       If drive torque is exerted on the follower disc 2f in the direction of the output torque M then the other scissor arm

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82f is loaded through the wedges 5f, 5f' and turns the locking elements 4f' and 4f'' tensioned by the output torque.

If as a result of torque on the output side the locking elements 4f, 4f' and 4f'', 4f''' are loaded by the output element 3f, then the radial stops 46f of the locking elements 4f, 4f' and 4f'', 4f''' are moved up to each other and displace the scissor arms 81f, 82f relative to each other accordingly. Since this movement must not be impeded by the wedges 5f, 5f' the wedge angle  $\alpha$  must be so great that the wedges 5f, 5f' can move outwards without self locking.

One embodiment with automatic play adjustment between a drive element 2g, an output element 3g and a load torque lock 1g without scissor arms is shown in Figure 9 in which the same function parts are marked with the same reference numerals as in Figure 8 so that for the description and explanation of the function of these parts reference is made to the illustration of Figure 8.

In this embodiment the locking elements 4g, 4g' and 4g'', 4g''' of two superposed pairs of locking elements have window-shaped recesses 44 (of which only the recess of the one locking element 4g was marked) in which wedges 5g, 5g' are mounted and adjoin with their wedge faces 51g, 51g' against the one or other side face of the recesses 44 of the superposed locking elements 4g, 4g' and 4g'', 4g'''. The wedges 5g, 5g' which are likewise guided in slide guides 20g, 20g' of the follower disc 2g by means of wedge guides 52g, 52g' press with their wedge faces 51g, 51g' directly against the locking elements 4g, 4g' and 4g'', 4g''' and thus cause an automatic play compensation as a result of tolerances and wear through the high surface pressure ~~whilst~~while simultaneously observing the torsion angle play which is required for functioning.

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Figure 10 shows a plan view and Figure 11 a longitudinal sectional view along the line XI-XI of Figure 10 through a load torque lock 1h which corresponds to the load torque lock 1f according to Figure 8.

In this arrangement instead of the springs 7f, 7f' which are provided in Figure 8 between the displacement housing 10 and the end sides of the wedges 5h, 5h' facing the displacement housing two wire springs 7h, 7h' are provided whose ends are supported in recesses 53h, 53h' and 54h, 54h' of the wedges 5h, 5h'. The ends of the wire springs 7h, 7h' adjoin with force locking engagement against the walls, nearer the output axis 30, of the recesses 53h, 53h' and 54h, 54h' of the wedges 5h, 5h' guided with wedge guides 52h, 52h' in slide guides of the follower disc 2h and cause a slight pretensioning of the wedges 5h, 5h' in the direction of the output axis 30 so that the scissor arms 81h, 82h are pressed apart analogous with the arrangement and description according to Figure 8 and their angled ends are brought to bear against the radial stops of the locking elements (not shown in further detail here).

An alternative load torque lock 1i to the load torque lock 1h according to Figures 10 and 11 is shown in Figure 12 and has instead of two wire springs for pretensioning the wedges 5i, 5i' a yoke or formed spring 7i whose angled ends 71i, 72i are mounted in recesses 55i, 55i' of the wedges 5i, 5i' and cause the wedge faces of the wedges 5i, 5i' to bear against the scissor arms 81i, 82i accordingly to compensate play. Also in this illustration of this embodiment elements having the same construction and same function are provided with the same reference numerals as with the embodiments already illustrated.

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Two further variations for an automatic play compensation between a drive element, an output element and a load torque lock with pairs of locking elements mounted one above the other in two planes are shown in Figures 13 to 16 each with the minimum and maximum play and with internal and external wedges.

The load torque lock 1k according to Figures 13 and 14 has analogous with the embodiments already described two locking elements 4k, 4k' and 4k'', 4k''' mounted in a displacement housing 10 in superposed planes of the load torque lock 1k as well as a drive element (not shown in further detail) whose slide guides 20k, 20k' are connected in positive locking engagement with the wedge guides 52k, 52k' of two wedges 5k, 5k', and an output element 3k which is rotatable about an output axis of the output axle 30.

The wedges 5k, 5k' are mounted between opposite expanding faces 41k to 41k''' of the locking elements 4k, 4k' and 4k'', 4k''' of each plane wherein the expanding faces 41k to 41k''' open towards the displacement housing 10 and the wedge faces 51k, 51k' adapted to the opening of the expanding faces 41k to 41k''' extend out towards the displacement housing 10 so that the wedges 5k, 5k' are mounted "on the outside". The opening angles of the expanding faces 41k, 41k' and 41k'', 41k''' and of the wedge faces 51k, 51k' are thereby different from each other so that a linear bearing contact is provided between the expanding faces 41k, 41k' and 41k'', 41k''' and the wedge faces 51k, 51k'.

The locking elements 4k, 4k' and 4k'', 4k''' of each plane are pressed apart by locking element springs 6k, 6k' mounted in recesses of the locking elements 4k, 4k' so that - as previously described - the expanding faces 41k, 41k' and 41k'', 41k''' adjoin the wedge faces 51k, 51k' and the

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clamping faces 43k, 43k' and 43k'', 43k''' adjoin the displacement housing 10.

5       Through the action of two wire, yoke or formed springs 7k, 7k' the wedges 5k, 5k' are pretensioned in the direction of the displacement housing 10 so that with maximum play the position of the wedges 5k, 5k' shown in Figure 13 is produced ~~whilst~~while minimum play is characterised by the position of  
10      the wedges 5k, 5k' shown in Figure 14.

The load torque lock 11 according to Figure 15 and 16 has analogous with the embodiment previously described two locking elements 41, 41' and 41'', 41''' mounted in a displacement housing 10 in superposed planes of the load torque lock 11 as  
15      well as a drive element (not shown in further detail) whose slide guides 201, 201' are connected with positive locking engagement with the wedge guides 521, 521' of two wedges 51, 51', and an output element 31 rotatable about an output axis  
of the output axle 30.

20      The wedges 51, 51' are mounted between the opposing expanding faces 411 to 411''' of the locking elements 41, 41' and 41'', 41''' of each plane wherein the expanding faces 411 to 411''' close towards the displacement housing 10 so that the wedges 51, 51' are arranged "on the inside", i.e. are  
25      enclosed by the expanding faces 411, 411' and 41'', 411''' of the brake elements 41, 41' and 41'', 41'''. The locking elements 41, 41' and 41'', 41''' of each plane are pressed apart by locking element springs 61, 61' mounted in recesses of the locking elements 41, 41' and 41'', 41''' so that - as  
30      previously described - the expanding faces 411, 411' and 411'', 411''' bear against the wedge faces 511, 511' and the clamping faces 431, 431' and 431'', 431''' bear against the displacement housing 10.

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The opening angles of the expanding faces 411, 411' and 411'', 411''' and of the wedge faces 511, 511' are also here different from each other so that a linear contact is produced between the expanding faces 411, 411' and 411'', 411''' and the wedge faces 511, 511'.

The wedges 51, 51' are pretensioned in the direction of the displacement housing 10 under the effect of two wire, yoke or form springs 71, 71' so that with maximum play the position of the wedges 51, 51' shown in Figure 15 is produced ~~whilst~~ while minimum play is characterised by the position of the wedges 51, 51' shown in Figure 16.

Further variations for compensating play between a drive element, an output element and a load torque lock with pairs of locking elements mounted one above the other in two planes are shown diagrammatically in Figures 17 and 18.

The part of a displacement device shown in Figure 17 having a load torque lock 1m has analogous with the embodiments illustrated previously, two pairs of locking elements 4m, 4m' mounted in a displacement housing 10 in superposed planes of the load torque lock 1m as well as a rod-like drive element 2m and an output element 3m which encloses the rod-like drive element 2m with play.

A locking element spring 6m is mounted at one end of the locking elements 4m, 4m' between opposing expanding faces 41m, 41m' of the locking elements 4m, 4m' of each plane and brings both the clamping faces 43m, 43m' of the locking elements 4m, 4m' to bear against the displacement housing 10 and also through rotation of the locking elements 4m, 4m' in the displacement housing 10 to bear against the contact bearing points A, B of the output element 3m. The clamping faces 43m, 43m, thereby adjoin the displacement housing 10 and through rotation of the locking elements 4m, 4m' in the



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circumferential direction adjoin the stop points A and B on the output element 3m.

5           A wedge 5m is provided as a play compensating device and with its wedge faces 5lm, 5lm' tapering towards the displacement housing 10 adjoins the expanding faces 43m, 43m' of the locking elements 4m, 4m' and is pushed through a bore 52m to guide the wedge 5m on to the rod-like drive element 2m and is guided through same. A spring 7m is mounted between  
10       the end face of the wedge 5m remote from the displacement housing 10 and the end face of the output element 3m facing this said end face, the spring 7m pretensioning the wedge 5m in the direction of the expanding faces 5lm, 5lm' and thus as  
15       a result of the configuration of the facing expanding faces 41m, 41m' of the locking element 4m, 4m' as well as of the wedge faces 5lm, 5lm' of the wedge 5m causes the locking elements 4m, 4m' to slide apart in parallel and bear radially in each plane against the displacement housing 10.

20           The wedge faces 5lm, 5lm' of the wedge 5m thus adjoin the expanding faces 41m, 41m' of the locking elements 4m, 4m' so that no self-locking action is produced between the locking elements 4m, 4m' and the wedge 5m. The wedge 5m is pressed back against the spring 7m under the effect of the locking  
25       element springs 6m and the resulting rotation of the locking elements 4m, 4m' in the displacement housing 10.

          If a drive torque is exerted on the drive element 2m against the output torque then this drive torque is first transferred to the wedge 5m since sufficient play is provided  
30       between the drive element 2m and the output element 3m. The wedge 5m is pressed with self-locking action by the drive element 2m against the locking elements 4m, 4m' and lifts the clamping faces 43m, 43m' of the locking elements 4m, 4m' slightly away from their bearing against the displacement  
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housing 10 so that the friction contact is eliminated or reduced and the drive element 2m as a result of overcoming the play between the drive element 2m and output element 3m comes to bear against the inner faces of the output element 3m. The drive torque is thereby transferred directly to the output element 3m in the rotary direction of the drive torque.

If however torque is exerted on the output element 3m then the output element 3m transfers, as a result of its bearing contact against points A and B on the locking elements 4m, 4m', the torque to the locking elements 4m, 4m' whereby the bearing contact of the clamping faces 43m, 43m' against the displacement housing 10 is intensified and thus torque transfer from the output element 3m to the drive element 2m is blocked.

Figure 18 shows an arrangement which is substantially similar to the embodiment according to Figure 17. As opposed to the embodiment according to Figure 17 however with the load torque lock 1n according to Figure 18 the wedge 5n is provided with a recess 52n into which an end of the drive element 2n engages and thereby guides the wedge 5n, and the wedge faces 51n, 51n' thereby expand towards the displacement housing 10 and adjoin expanding faces 41n, 41n' of the locking elements 4n, 4n' which open correspondingly towards the displacement housing, i.e. the distance between the expanding faces 41n, 41n' of the locking elements 4n, 4n' increases towards the displacement housing 10. The expanding faces 41n, 41n' are adjoined by the wedge faces 51n, 51n' of the wedge 5n under the action of a weak spring 7n which is mounted between the displacement housing 10 and the end face of the wedge 75n facing the displacement housing 10.

Analogous with the arrangement according to Figure 17 the wedge faces 51n, 51n' of the wedge 5n thus adjoin the

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expanding faces 41n, 41n' of the locking elements 4n, 4n' so that no self locking action is produced between the locking  
5 elements 4n, 4n' and the wedge 7n. The wedge 5n is pressed back against the spring 7n under the action of the locking element spring 6n with the resulting rotation of the locking elements 4n, 4n' in the displacement housing 10.

10       If a drive torque is exerted against the output torque onto the drive element 2n then this drive torque is first transferred to the wedge 5n since sufficient play is provided between the drive element 2n and the output element 3n. The wedge 5n is pressed with self locking action by the drive  
15 element 2n against the locking elements 4n, 4n' and lifts the clamping faces 43n, 43n' of the locking elements 4n, 4n' slightly away from their bearing contact against the displacement housing 10 so that the friction connection is lifted or reduced and the drive element 2n as a result of  
20 overcoming the play between the drive element 2n and the output element 3n comes to bear against the inside faces of the output element 3n whereby the drive torque is transferred directly to the output element 3n in the rotary direction of the drive torque.

25       If however torque is exerted on the output element 3n then the output element 3n as a result of the contact bearing of the output element 3n and locking elements 4n, 4n' against the points A and B transfers the torque to the locking elements 4n, 4n' whose clamping faces 43n, 43n' intensify their contact bearing against the displacement housing 10 so  
30 that torque transfer from the output element 3n to the drive element 2n is blocked.

All the displacement devices described above have the common basic function according to which with drive torque acting in the direction of the output torque the lock caused

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by the locking element is lifted but remains latently active  
so that an immediate locking takes place when the drive torque  
5      is lifted. If however the drive torque acts against the  
output torque then the lock is lifted and the drive torque is  
introduced into the output. A slight lifting or circular  
rotation of the locking element thereby takes place and then  
an immediate renewed bearing contact against the displacement  
10     housing.

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ABSTRACT OF THE DISCLOSURE

A displacement device for producing a rotational movement with an output element ~~3a~~ adjustable in angle by operating a drive element ~~2a~~ ~~has a~~. A load torque lock ~~1a~~ mounted between the drive element ~~2a~~ and the output element ~~3a~~ and ~~which blocks~~, with force locking connection, torque introduced on the output side and transfers torque introduced on the drive side to the output element ~~3a~~. Between the drive element ~~2a~~ and the load torque lock ~~1a~~ and/or between the output element ~~3a~~ and the load torque lock ~~1a~~ is a play compensating device ~~5a~~ which compensates the torsion angle play between the drive element ~~2a~~, the output element ~~3a~~ and the load torque lock ~~1a~~. The displacement device is used in particular for window lifters or seat adjusters of vehicles. ~~(Figure 1).~~

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**Amendments to the Drawings:**

The attached sheets of drawings include changes to Figs. 1, 2a, 3a, 4, 5, 7a and 7b. These sheets, which include Figs. 1, 2a, 2b, 2c, 3a, 3b, 4, 5, 7a and 7b replace the original sheets including Figs. 1, 2a, 2b, 2c, 3a, 3b, 4, 5, 7a and 7b. FIG. 1a is added to show a side sectional view of FIG. 1.

Attachment:      Replacement Sheets  
                    Annotated Sheet Showing Changes

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**REMARKS/ARGUMENTS**

This application is a continuation of U.S. Serial No. 09/592,485 ("the parent application"). The parent application received a Notice of Allowance on December 24, 2002. Subsequently, Applicant filed a Petition to withdraw from issue in order to file an information disclosure statement. The Petition was granted and the application was forwarded to the Examiner for consideration of the Information Disclosure Statement.

A new Office action was issued on May 27, 2003 rejecting all claims as anticipated by DE 3415692. In response, this continuation application was filed on November 28, 2003.

Claims 1-29 have been amended to place them in the same condition as they existed at the time of the issuance of the Notice of Allowance in the parent application. In addition, claim 1 has been amended to recite that the load torque lock "includes rigid locking elements."

The specification and drawings have also been amended to place them in the same condition as they existed at the time of the issuance of the Notice of Allowance in the parent application. Due to the number of amendments, a Substitute Specification pursuant to 37 CFR § 1.125 and MPEP § 608.01(q) is submitted herewith to facilitate the prosecution of this application. The Substitute Specification is accompanied by a marked-up copy showing the changes between the original application, as filed, and the Substitute Specification. It is believed that the Substitute Specification does not contain any new matter and includes the same changes as are indicated in the

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marked-up copy. Applicant respectfully requests that the Substitute Specification be entered in this case.

With regard to the drawings, Fig. 1 has been amended to depict play compensation direction arrows C and C'. These are described on page 10 of the Substitute Specification as being "circular against the expanding faces." Fig. 1 has also been amended to depict slide guide 21a', output axle axis E, a rotation direction D of the drive lever, section line 1a-1a and gaps F and F'. Fig. 1a is added to show a side sectional view of Fig. 1. Figs. 2a, 3a, 4, 5, 7a and 7b have been amended to provide English translations to the foreign language words.

With regard to the May 27, 2003 Office action, the drawings were objected to for two reasons. In paragraph 5a on page 3 of the Office action, the Examiner states that Fig. 2c is depicted as showing wedge 5a after it has slipped from the position shown in Fig. 2b. Applicant respectfully disagrees. Fig. 2b shows the force and friction conditions in the event of load on the drive side. (Page 12, lines 5-6 of the new Substitute Specification) Fig. 2c shows the force and friction conditions in the event of load on the output side. (Page 12, lines 28-29 of the new Substitute Specification) These are two different conditions which do not depend on each other.

In paragraph 5b on page 3 of the Office action, the Examiner indicates that the plane upon which the sectional view in Fig. 1a is taken is not indicated in Fig. 1. Fig. 1 has been amended to include section line 1a-1a.

In paragraph 7 on page 3 of the Office action, the abstract of the disclosure is objected to because its first sentence is a run-on sentence. A substitute abstract is submitted herewith on a separate sheet to address this.



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In paragraph 8a on pages 3-4 of the Office action, the description on page 10, line 18 is considered contradictory and confusing. (The Office action citation corresponds to Page 9, line 17 of the new Substitute Specification.) The specification has been amended to address this.

It is noted that the passage in question refers to the friction conditions between the expanding faces 41a, 41a' and the wedge faces 51a, 51a' and the friction conditions between the wedge guide 52a and the slide guide 20a.

On the one hand, said friction conditions are such that when wedge 5a starts to move due to torque load of the drive lever 2a, the locking elements 4a, 4a' start to move concurrently because there is no gap between wedge faces 51a, 51a' and expanding faces 41a, 41a' that has to be overcome. This corresponds to the normal operating status of the displacement device due to torque load and should not be mistaken with the movement of the locking elements 4a, 4a' due to play compensation. On the other hand, said friction conditions are such that they allow the locking elements 4a, 4a' to move in a play compensation direction without being impeded by the wedge 5a. That means, that friction conditions are such that in the rest state, the locking elements 4a, 4a' are pressed by wedge 5a against the displacement housing 10 by aid of the spring 7a.

In other words, when load torque is applied to drive lever 2a, the locking elements 4a, 4a' are entrained by wedge 5a. Concurrently, the locking elements 4a, 4a' start to move in one of the two possible directions of rotation. That means both locking elements 4a, 4a' move in the same rotational direction which corresponds to the rotational direction of the drive lever

2a. During play compensation both locking elements 4a, 4a' counter rotate. Play compensation movement takes place due to abrasion of the locking elements 4a, 4a' (discussed in more detail in connection with torsion angle play).

In paragraph 8b on page 4 of the Office action, the Examiner requests clarification as to the "function" on page 11, line 6 (see page 10, line 3 of the new Substitute Specification). The referenced function is the "entrained"/"pressed" function referenced on page 9, line 28 and page 9, line 31 of the new Substitute Specification prior to the amendment herein. In other words, this function means, on the one hand, the entrainment of the locking elements 4a, 4a' and on the other hand, the possibility of the expanding face for 41a, 41a' and the wedge faces 51a, 51a' to slide along each other, which correspond to the pressing during play compensation.

In paragraph 8c on page 4 of the Office action, the Examiner requests clarification of the structural details of output element 3a. In particular, the Examiner indicates that the output element 3a has two bulbous profiles which appear to be a "necessary" feature. Applicant believes that the invention should not be limited to this feature. As an example, the contact points A, A' function to direct a load torque introduced at the output side into the locking elements 4a, 4a' as stated on page 11, starting at line 7. Thus, the shape of the output element 3a depends on the shape of the locking elements 4a, 4a'. Regarding the gaps F, F' on page 11, line 5, a minimum torsion angle play must be present. This is common knowledge to one skilled in the art (discussed in more detail below in connection with torsion angle play).

In paragraph 8d on page 4 of the Office action, the Examiner states that the paragraph starting on page 12, line 19 is a run-on sentence. The specification has been amended to address this.

In paragraph 9 on page 5 of the Office action, claim 1 is objected to regarding the terms "output side" and "drive side". Claim 1 has been amended to address this.

In paragraph 10 on page 5 of the Office action, claims 1-8 and 29 are rejected under 35 U.S.C. §112, second paragraph, as being indefinite for failing to particularly point out and distinctly claim the subject matter which applicant regards as the invention. In particular, the Examiner refers to the limitation "a torsion angle play."

The present application discloses two types of torsion angle play, one type of which is compensated and the other type of which is not compensated. The object of the present invention is to provide a displacement device with "optimum" torsion angle play between the drive element, an output element, and a load torque block. See page 2, lines 23-26 of the new Substitute Specification.

It can be seen from Fig. 1, for example, that between the output element 3a and the locking elements 4a, 4a', there is a gap (reference letters F, F'). With reference to the gap, the displacement device of Fig. 1 works as follows:

After actuating drive element 2a, for instance clockwise, wedge face 51a' of the wedge 5a is pressed without play against the expanding face 41a' of the locking element 4a'. Then wedge 5a and locking element 4'a start to move clockwise in a circumferential direction until claws 31, 32 engage with slide grooves 21a', 21a. After this engaging, the output element 3a

also rotates about axle 30. See page 10, lines 10-26 of the new Substitute Specification.

The torsion angle, which wedge guide 5a and locking element 4a' cover before claws 31, 32 engage with slide guide 21a', 21a, is a necessary torsion angle play, because with this arrangement, the stiction between the locking elements 4a, 4a' and the inner face of the housing 10 is overcome and then, the output element 3a is actuated. With no angle play between input and output, load torque has to be higher and all elements are much more strained. This necessary torsion angle play corresponds to the gap between claws 31, 32 and slide guides 21a', 21a. It is not compensated.

Other types of torsion angle play in the displacement device, however, are compensated, in particular, in Fig. 1, by the wedge guide 5a. Adjustment of the wedge guide 5a takes place as follows:

In a neutral position, the locking elements 4a, 4a' are clamped by spring 6a between the inner face of the housing 10 and points A, A' of the output element 3a. The wedge 5a abuts against the locking element 4a, 4a' without play.

During operation of the displacement device, the locking faces 43a, 43a' are highly strained and therefore abraded. Thus the neutral position of the locking elements 4a, 4a' will change due to the pressing force of the spring 6a, i.e., as locking faces 43a, 43a' are abraded, the locking elements 4a, 4a' move in a circumferential direction towards wedge 5a to get clamped once more between the inner face of the housing 10 and the output element 3a. Because the friction value between the locking elements 4a, 4a' and the wedge 5a is small, the wedge 5a is pressed radially by the locking elements 4a, 4a' more and

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more towards the inner face of the housing 10, when locking faces 43a, 43a' get more and more abraided. Thus wedge 5a always abuts against locking elements 4a, 4a' without play.

In comparison, if wedge 5a was fixed in its radial position, a gap would be required between the wedge 5a and the locking elements 4a, 4a' to let the locking elements 4a, 4a' get clamped when the locking faces 43a, 43a' are abraided. Thus such a gap would cause a large idling path of wedge 5a and therefore of drive lever 2a. This gap is the torsion angle play that is compensated by the present arrangement. Support for the recitation in the claims is found in the new Substitute Specification at page 2, line 31 - page 4, line 12.

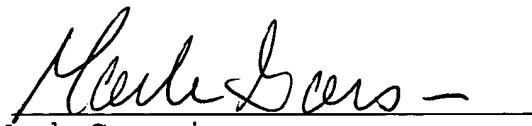
In paragraph 11 on page 5 of the Office action, claim 1 is rejected under 35 U.S.C. 102(b) as being anticipated by DE 34 15 692. As noted above, claim 1 has been amended to recite that the load torque lock includes "rigid locking elements." The equivalent of DE 34 15 692 to the locking elements of the present application is a spiral torsion spring 33, which engages the inner surface of a brake drum 30 with friction grip. The spiral torsion spring is not a rigid locking element. Accordingly, it is not believed that claim 1 is anticipated by DE 34 15 692.

In view of the above, Applicant respectfully requests reconsideration of the application and allowance of claims 1-29. If the Examiner believes that a telephone conference with

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Applicant's attorney might expedite the prosecution of the application, he is invited to call at the telephone number indicated below.

Respectfully submitted,  
CHRISTIE, PARKER & HALE, LLP

By   
Mark Garscia  
Reg. No. 31,953  
626/795-9900

MEG/cks  
CKS PAS576810.1--\*-06/20/05 10:28 AM



Fig. 1

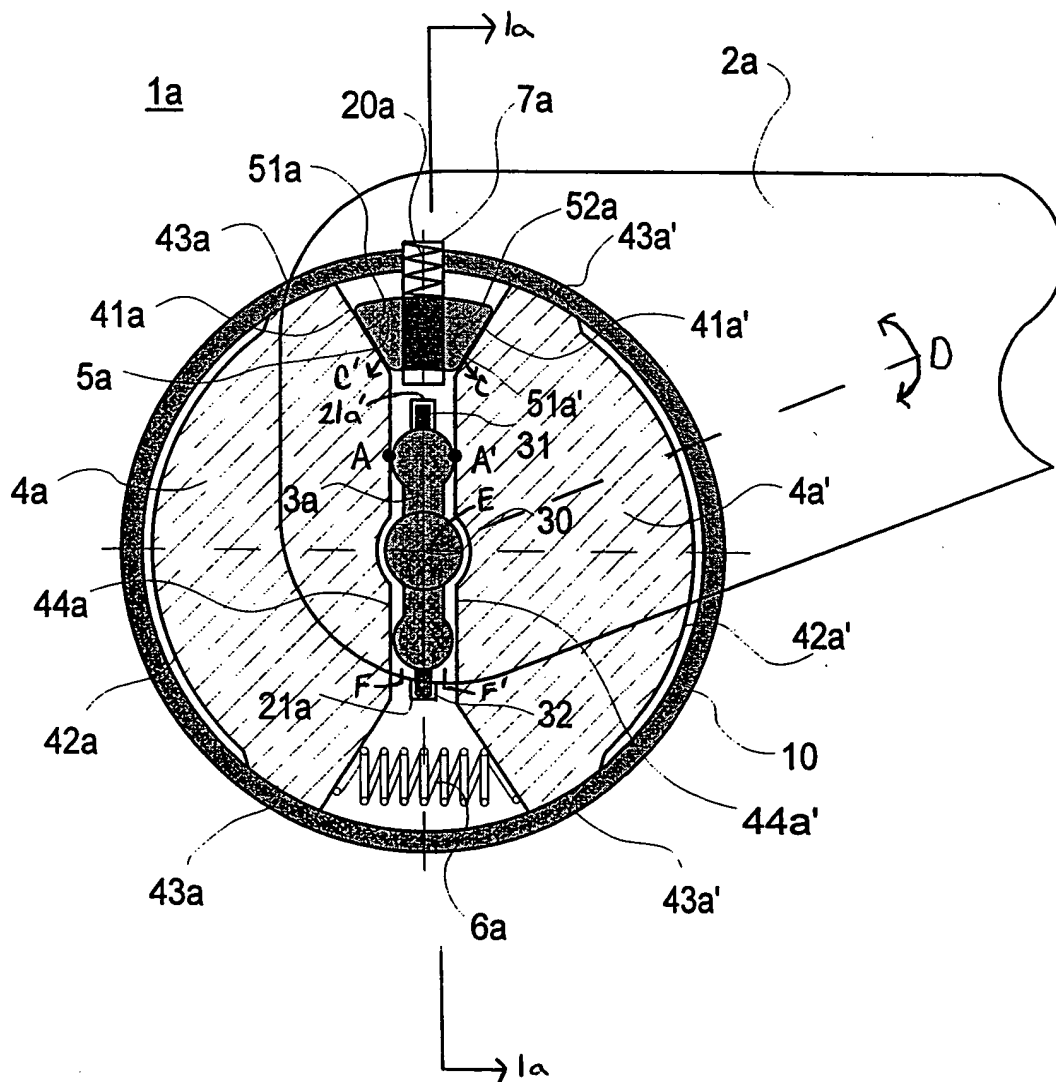


Fig. 2a

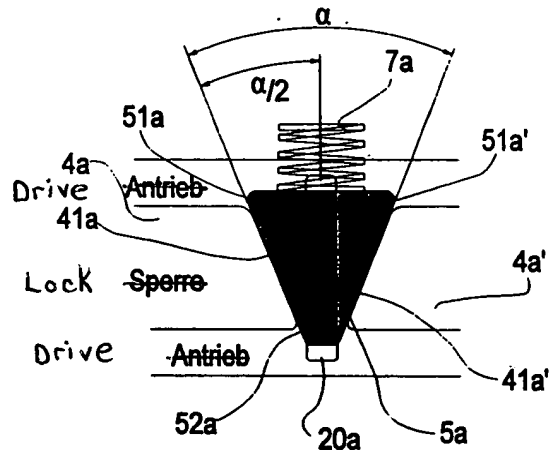


Fig. 2b

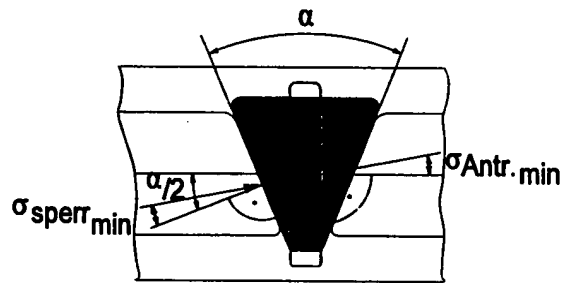


Fig. 2c

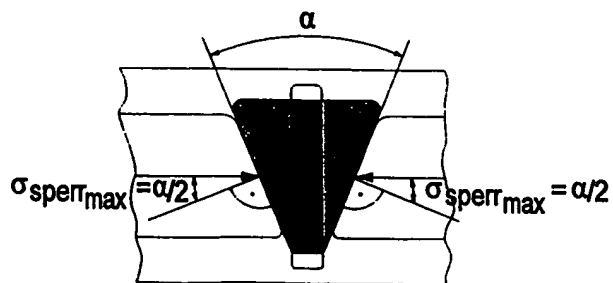




Fig. 3a

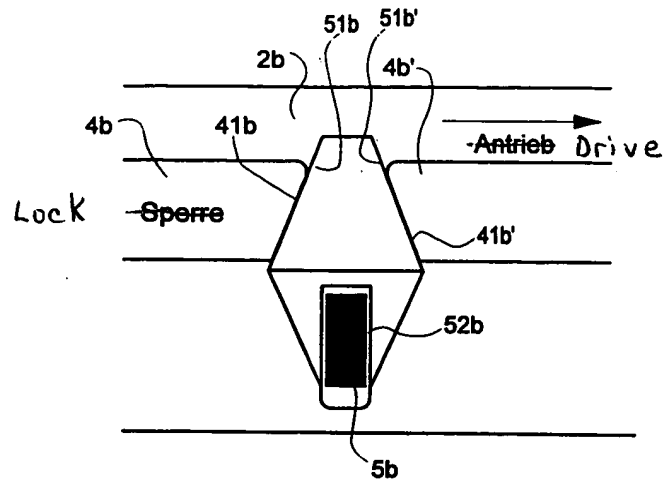


Fig. 3b

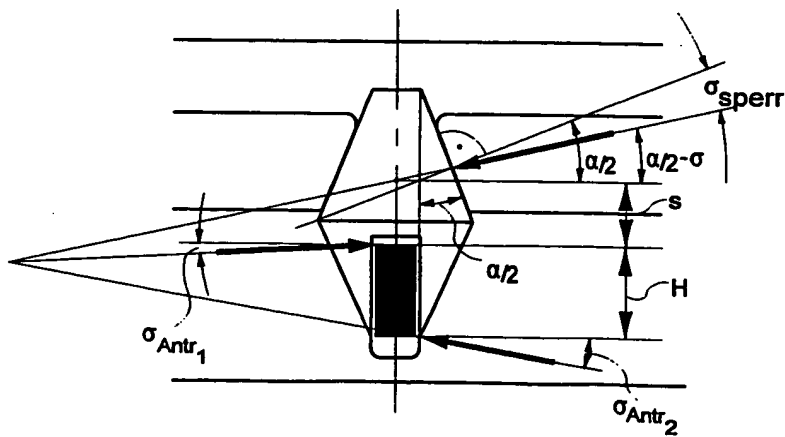


Fig. 4

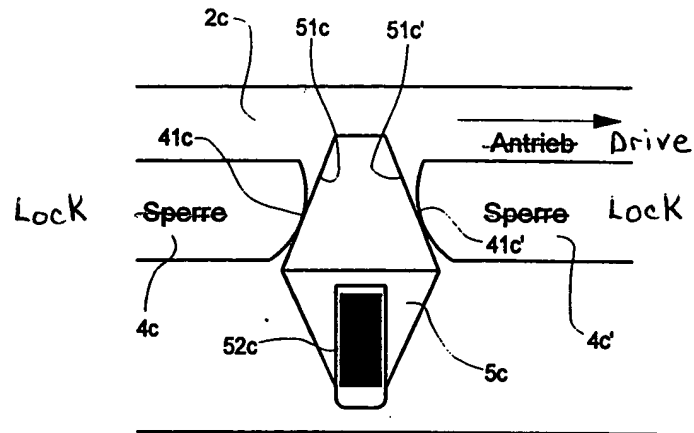


Fig. 5

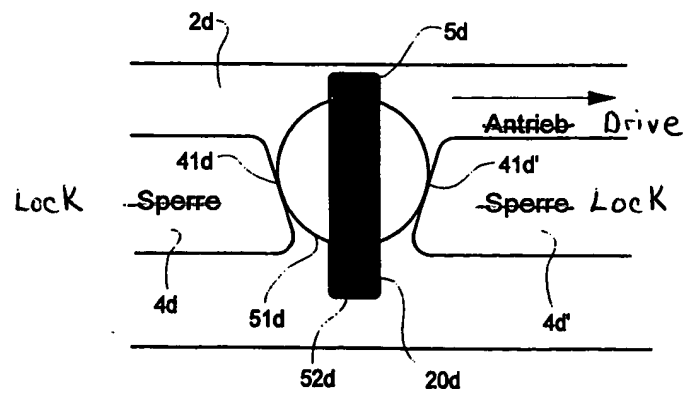


Fig. 7a

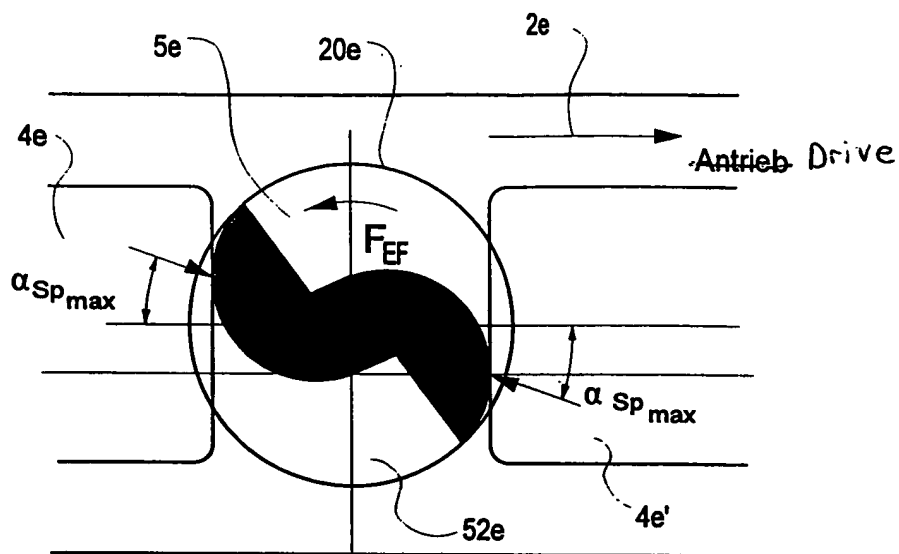


Fig. 7b

